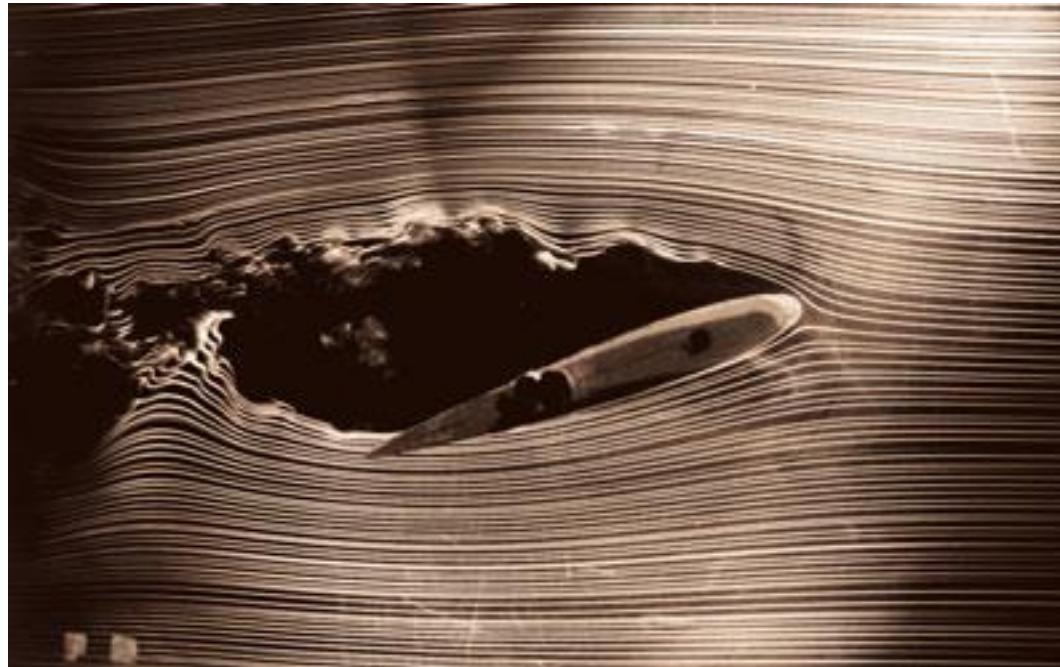


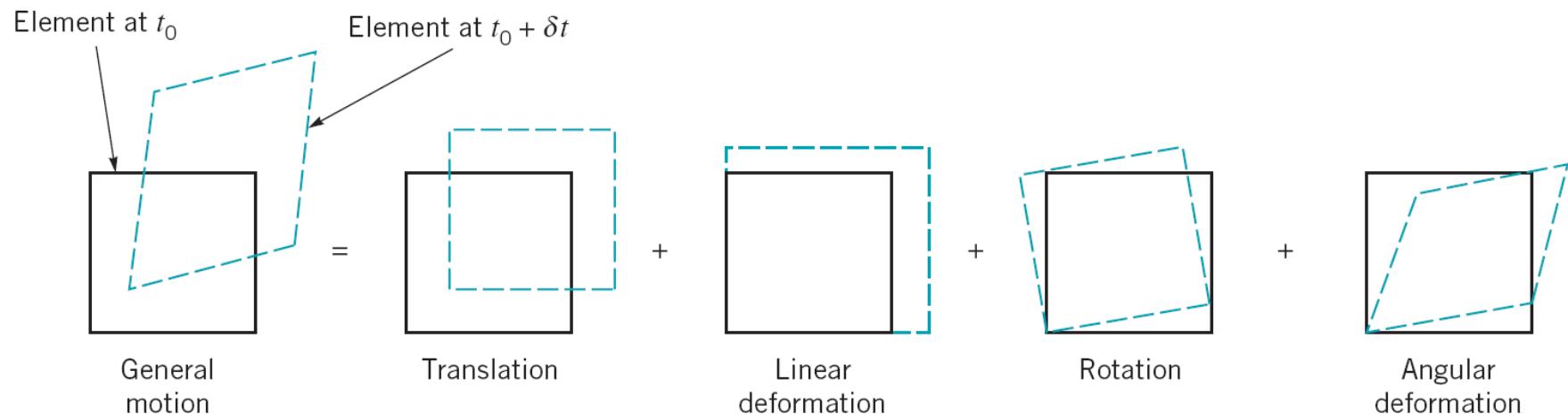
# Differential analysis of fluid flow



Sometimes the control volume of interest is infinitesimally small  
(a point in space rather than to a 2D or 3D volume)

→ Differential analysis rather than finite control volume analysis

# Types of motion and deformation for a fluid element.



# Velocity and acceleration field

Velocity:  $\vec{V} = u\vec{i} + v\vec{j} + w\vec{k}$

Acceleration:  $\vec{a} = \frac{\partial \vec{V}}{\partial t} + u\frac{\partial \vec{V}}{\partial x} + v\frac{\partial \vec{V}}{\partial y} + w\frac{\partial \vec{V}}{\partial z}$

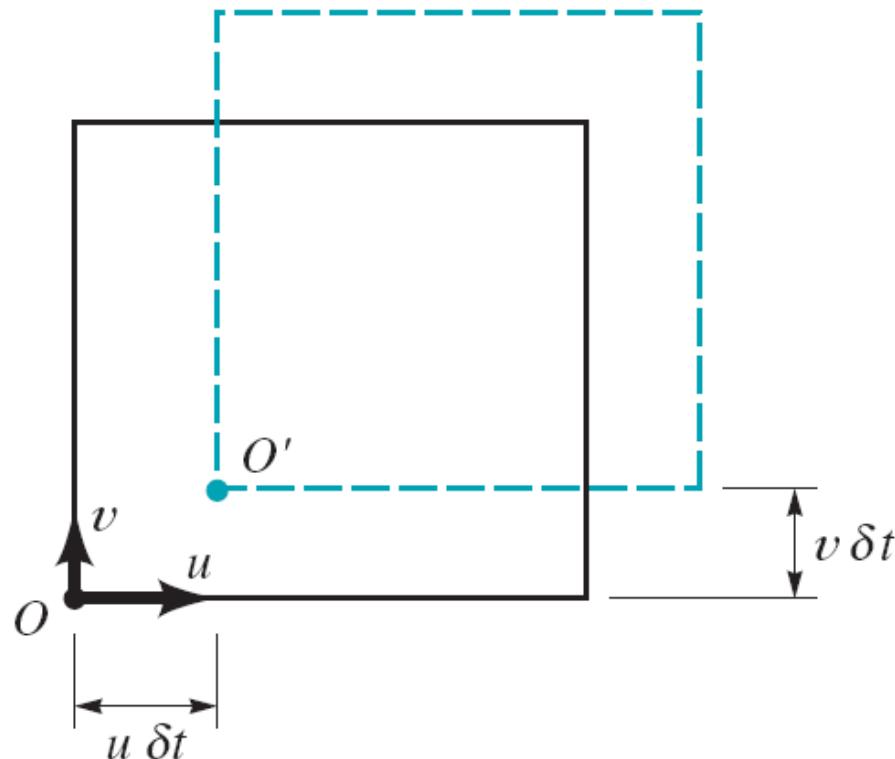
The acceleration is concisely expressed as:  $\vec{a} = \frac{D\vec{V}}{Dt}$

where the operator  $\frac{D(\cdot)}{Dt} = \frac{\partial(\cdot)}{\partial t} + u\frac{\partial(\cdot)}{\partial x} + v\frac{\partial(\cdot)}{\partial y} + w\frac{\partial(\cdot)}{\partial z}$

is termed **material derivative**. In vector notation:  $\frac{D(\cdot)}{Dt} = \frac{\partial(\cdot)}{\partial t} + (\vec{V} \cdot \vec{\nabla})(\cdot)$

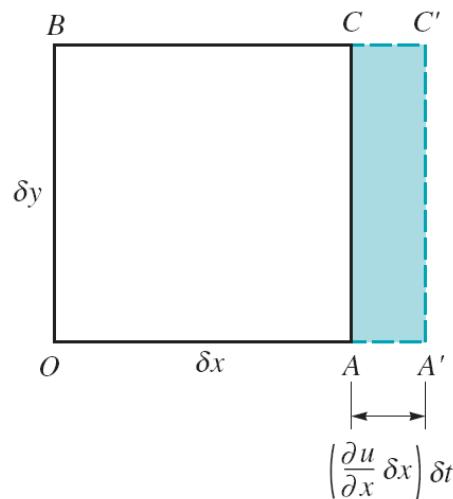
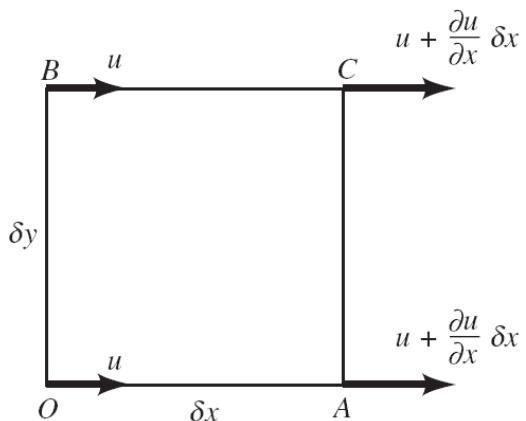
where the gradient operator is  $\vec{\nabla}(\cdot) = \frac{\partial(\cdot)}{\partial x}\vec{i} + \frac{\partial(\cdot)}{\partial y}\vec{j} + \frac{\partial(\cdot)}{\partial z}\vec{k}$

# Translation of a fluid element.



If the velocity,  $V$ , is the same for all fluid elements, we have **translation** without deformation

# Linear deformation of a fluid element.



If velocity gradients are present  
→ deformation

Fluid element volume:  $\delta V = \delta x \delta y \delta z$

Change in  $\delta V = \left[ \left( \frac{\partial u}{\partial x} \delta x \right) \delta t \right] \delta y \delta z$

Rate of change of volume per unit volume:

$$\frac{1}{\delta V} \frac{d(\delta V)}{dt} = \frac{1}{\delta x \delta y \delta z} \lim_{\delta t \rightarrow 0} \frac{\frac{\partial u}{\partial x} \delta x \cdot \delta y \cdot \delta z \delta t}{\delta t} = \frac{\partial u}{\partial x}$$

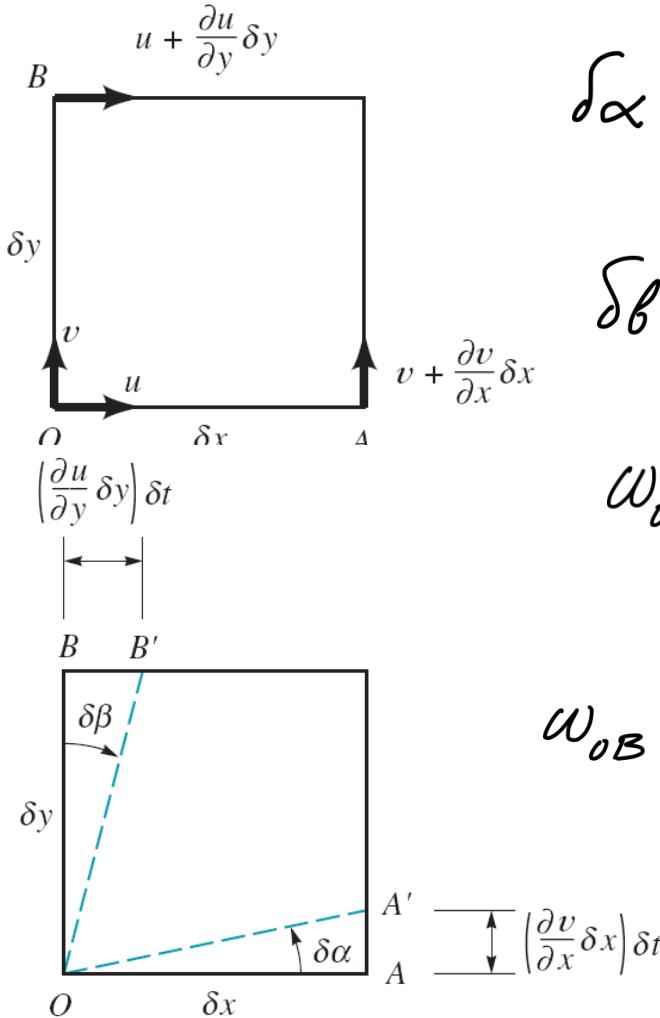
In general,

$$\frac{1}{\delta V} \frac{d(\delta V)}{dt} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = \vec{\nabla} \cdot \vec{v}$$

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Volumetric dilatation rate

# Angular motion and deformation of a fluid element.



$$\delta \alpha \simeq \tan \alpha = \frac{\frac{\partial v}{\partial x} \delta x \delta t}{\delta x} = \frac{\partial v}{\partial x} \delta t$$

$$\delta \beta \simeq \tan \beta = \frac{\frac{\partial u}{\partial y} \delta y \delta t}{\delta y} = \frac{\partial u}{\partial y} \delta t$$

$$\omega_{OA} = \lim_{\delta t \rightarrow 0} \frac{\delta \alpha}{\delta t} = \frac{\partial v}{\partial x} \quad \text{if } \frac{\partial v}{\partial x} > 0 \rightarrow \text{CCW}$$

$$\omega_{OB} = \lim_{\delta t \rightarrow 0} \frac{\delta \beta}{\delta t} = \frac{\partial u}{\partial y} \quad \text{if } \frac{\partial u}{\partial y} > 0 \rightarrow \text{CW}$$

By convention:  
 CCW is positive

# Rotation vector and vorticity

Definition of rotation:  $\omega_z = \frac{1}{2} \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right)$

Similarly:  $\omega_x = \frac{1}{2} \left( \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right)$

$$\omega_y = \frac{1}{2} \left( \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right)$$

$$\vec{\omega} = \omega_x \vec{i} + \omega_y \vec{j} + \omega_z \vec{k}$$

$$\vec{\omega} = \frac{1}{2} \operatorname{curl} \vec{v} = \frac{1}{2} \vec{\nabla} \times \vec{v}$$

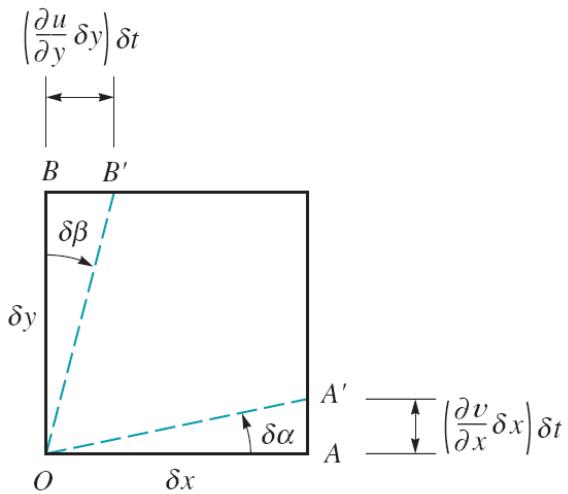
$$\frac{1}{2} \vec{\nabla} \times \vec{v} = \frac{1}{2} \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ u & v & w \end{vmatrix}$$

$$= \frac{1}{2} \left( \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) \hat{i} + \frac{1}{2} \left( \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right) \hat{j} + \frac{1}{2} \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) \hat{k}$$

Define vorticity  $\vec{j} = 2 \vec{\omega} = \vec{\nabla} \times \vec{v}$

Remarks: a) if  $\omega_{0A} = -\omega_{0B}$  or  $\frac{\partial u}{\partial y} = -\frac{\partial v}{\partial x}$

→ rotation as an undeformed block;  
otherwise: angular deformation



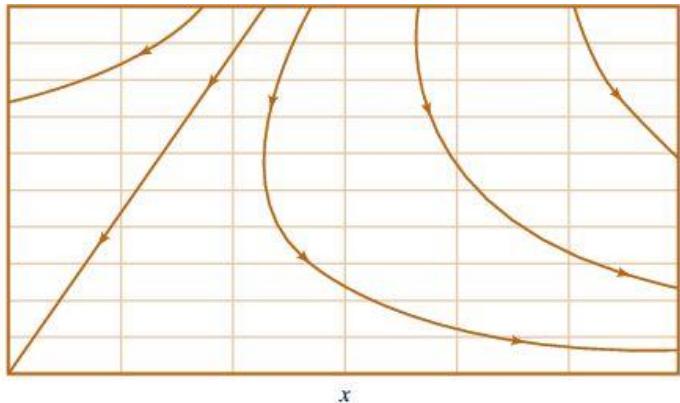
b) When  $\frac{\partial u}{\partial y} = \frac{\partial v}{\partial x}$

$$\omega_z = \left( \frac{\partial u}{\partial y} - \frac{\partial v}{\partial x} \right) = 0$$

rotation around z-axis is zero

In general, when  $\vec{\nabla} \times \vec{V} = 0 \rightarrow \vec{\omega} = \vec{\gamma} = 0$   
 → Irrotational flow

# Example: vorticity



Flow field with  $u = 4xy$   
 $v = 2(x^2 - y^2)$   
 $w = 0$

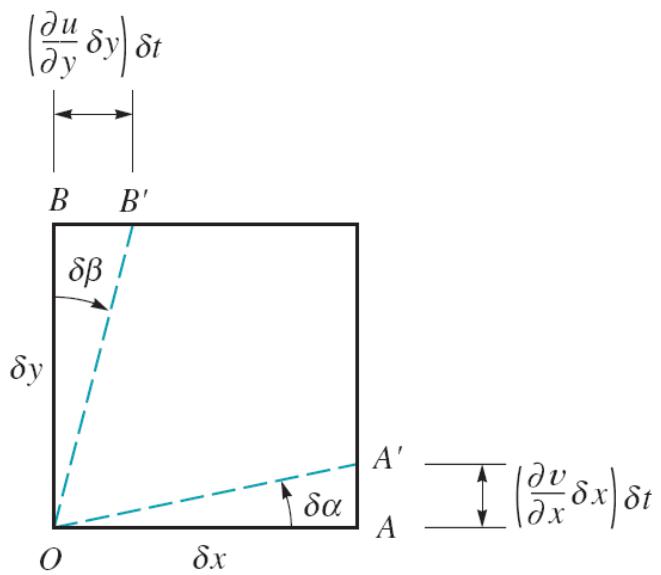
Is the flow field irrotational?

This is a 2-D flow field ( $w=0$ ). Hence  
 $\omega_x = \omega_y = 0$  (check!)

$$\omega_z = \frac{1}{2} \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) = \frac{1}{2} (4x - 4x) = 0$$

The flow field is irrotational.

# Angular deformation and shearing strain



Rate of angular deformation

The change in the original right angle ( $90^\circ$ ) between  $OA$  and  $OB$ ,  $\delta\gamma$

$$\delta\gamma = \delta\alpha + \delta\beta$$

Rate of change of  $\delta\gamma$  or shearing strain,  $j$ , is

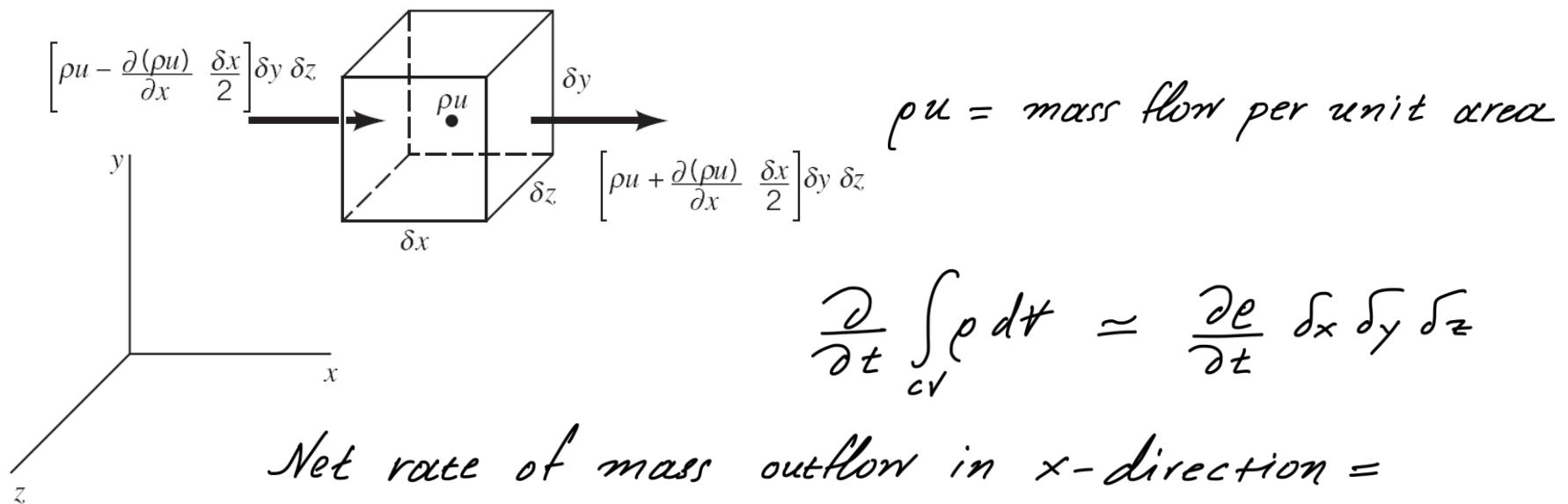
$$\lim_{\delta t \rightarrow 0} \frac{\delta j}{\delta t} = \lim_{\delta t \rightarrow 0} \left[ \frac{\frac{\partial v}{\partial x} \delta t + \frac{\partial u}{\partial y} \delta t}{\delta t} \right]$$

$$\Rightarrow j = \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y}$$

## Differential form of the conservation of mass equation.

Conservation of mass:  $\frac{\partial}{\partial t} \int_{cv} \rho dt + \int_{cs} \vec{\rho} \cdot \vec{n} dA = 0 \quad (1)$

Differential form of the continuity equation



$$\frac{\partial}{\partial t} \int_{cv} \rho dt \simeq \frac{\partial \rho}{\partial t} \delta x \delta y \delta z \quad (2)$$

Net rate of mass outflow in  $x$ -direction =

= rate of mass outflow - rate of mass inflow

$$= \left[ \rho u + \frac{\partial(\rho u)}{\partial x} \frac{\delta x}{2} \right] \delta y \delta z - \left[ \rho u - \frac{\partial(\rho u)}{\partial x} \frac{\delta x}{2} \right] \delta y \delta z$$

$$= \frac{\partial(\rho u)}{\partial x} \delta x \delta y \delta z$$

$$x\text{-direction: } \frac{\partial(\rho u)}{\partial x} \delta x \delta y \delta z$$

$$y\text{-direction: } \frac{\partial(\rho v)}{\partial y} \delta x \delta y \delta z$$

$$z\text{-direction: } \frac{\partial(\rho w)}{\partial z} \delta x \delta y \delta z$$

Net rate of mass outflow:

$$\underline{\left[ \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial(\rho w)}{\partial z} \right] \delta x \delta y \delta z} \quad (3)$$

$$\underline{(1), (2) \text{ and } (3) \Rightarrow \frac{\partial \rho}{\partial t} + \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial(\rho w)}{\partial z} = 0}$$

Conservation of mass or continuity

In vector notation:

$$\underline{\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v}) = 0}$$

Special cases: 1) Steady flow  $\vec{\nabla} \cdot (\rho \vec{v}) = 0$

$$\text{or } \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial(\rho w)}{\partial z} = 0$$

2) Incompressible flow ( $\rho = ct$ )

$$\vec{\nabla} \cdot \vec{v} = 0 \quad \text{or } \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

## Example: 3D steady, incompressible flow

Velocity components in a steady and incompressible flow field:

$$u = x^2 + y^2 + z^2$$

$$v = xy + yz + z$$

$$w = ?$$

Solution: To satisfy the continuity equation for steady and incompressible flow:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

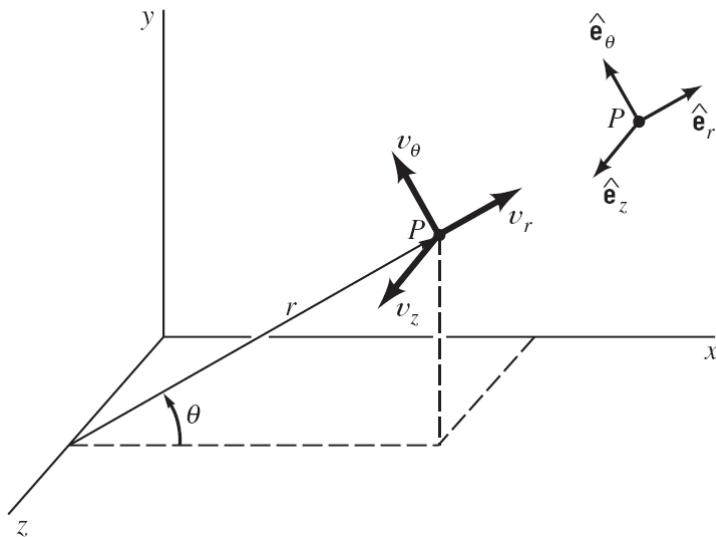
$$\Rightarrow 2x + (x+z) + \frac{\partial w}{\partial z} = 0$$

$$\Rightarrow \frac{\partial w}{\partial z} = -2x - (x+z) = -3x - z$$

$$\Rightarrow w = -3xz - \frac{1}{2}z^2 + f(x, y)$$

need more  
info to define

## Velocity components in cylindrical polar coordinates.



Continuity eq. in cylindrical coordinates:

$$\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial (r \rho v_r)}{\partial r} + \frac{1}{r} \frac{\partial (\rho v_\theta)}{\partial \theta} + \frac{\partial (\rho v_z)}{\partial z} = 0$$

For incompressible flow (steady or unsteady):

$$\frac{1}{r} \frac{\partial (r v_r)}{\partial r} + \frac{1}{r} \frac{\partial v_\theta}{\partial \theta} + \frac{\partial v_z}{\partial z} = 0$$

# Stream function

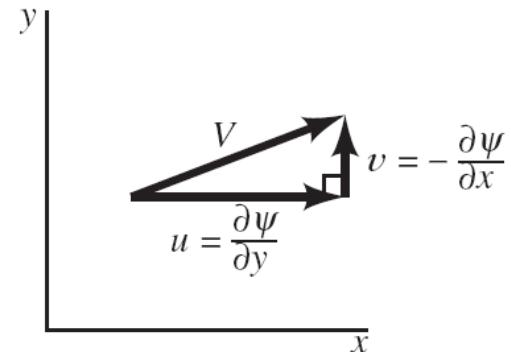
For 2-D flow  $\vec{V} = u\hat{i} + v\hat{j}$

For steady, incompressible, 2-D flow,  
the continuity equation is:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

Define **stream function**  $\Psi(x, y)$  such as

$$u = \frac{\partial \Psi}{\partial y} \quad \text{and} \quad v = -\frac{\partial \Psi}{\partial x}$$



Continuity: 
$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = \frac{\partial}{\partial x} \left( \frac{\partial \Psi}{\partial y} \right) + \frac{\partial}{\partial y} \left( -\frac{\partial \Psi}{\partial x} \right)$$
$$= \frac{\partial^2 \Psi}{\partial x \partial y} - \frac{\partial^2 \Psi}{\partial x \partial y} \equiv 0$$

$\therefore$  When  $\Psi$  exists  $\Rightarrow$  continuity is satisfied

# Stream function property #1

Lines along which  $\Psi = ct$  are streamlines

Streamline: line tangent to  $\vec{V}$

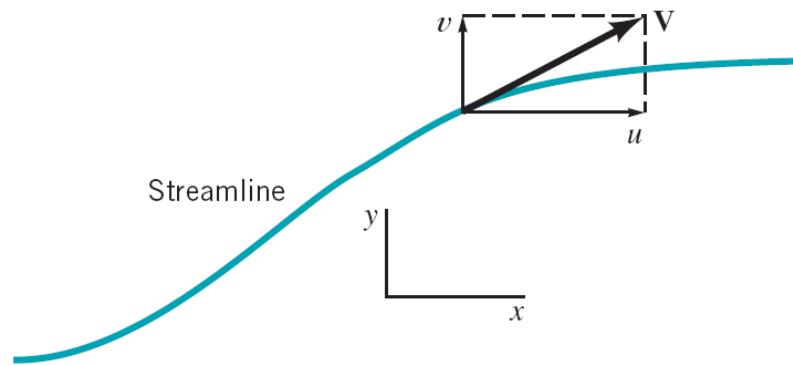
$$\frac{dy}{dx} = \frac{v}{u}$$

$$\begin{aligned} d\Psi &= \frac{\partial \Psi}{\partial x} dx + \frac{\partial \Psi}{\partial y} dy \\ &= -v dx + u dy \end{aligned}$$

When  $\Psi = ct \Rightarrow d\Psi = 0$

$$\Rightarrow -v dx + u dy = 0$$

$$\Rightarrow \underline{\underline{\frac{dy}{dx} = \frac{v}{u}}} \quad \text{streamline!}$$



Plot  $\Psi(x, y)$  to visualize the flow field

Note:  $\Psi$  defined within a constant.

# Stream function property #2

Change in the value of  $\Psi$  between two streamlines equals the volume rate of flow

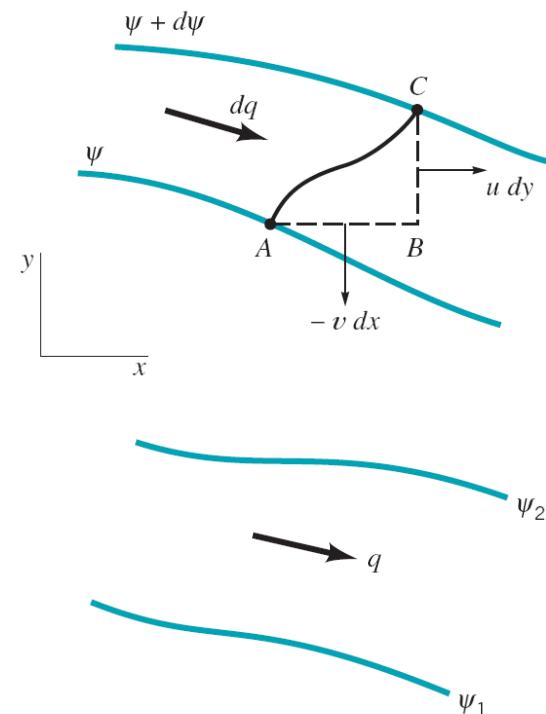
Flow never crosses streamlines  $\vec{V} \parallel \Psi$

$$dq = -v dx + u dy$$

inflow      outflow

$$\Rightarrow dq = \frac{\partial \Psi}{\partial x} dx + \frac{\partial \Psi}{\partial y} dy = d\Psi$$

$$\Rightarrow q = \int_{\Psi_1}^{\Psi_2} d\Psi = \Psi_2 - \Psi_1$$



Note: if  $\Psi_2 > \Psi_1 \rightarrow$  flow from left to right  
if  $\Psi_2 < \Psi_1 \rightarrow$  flow from right to left

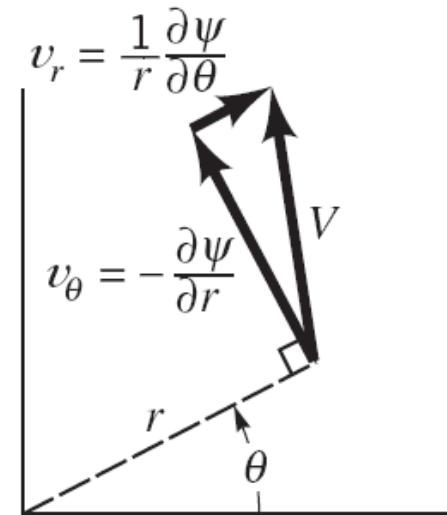
# Stream function in cylindrical coordinates

In cylindrical coordinates:

Continuity:  $\frac{1}{r} \frac{\partial(r v_r)}{\partial r} + \frac{1}{r} \frac{\partial v_\theta}{\partial \theta} = 0$

$$v_r = \frac{1}{r} \frac{\partial \psi}{\partial \theta}$$

$$v_\theta = - \frac{\partial \psi}{\partial r}$$



# Example: stream function

Steady, incompressible 2-D flow with:

$$u = 2y$$

$$v = 4x$$

a)  $\psi = ?$

b) Streamlines?

c) Direction of flow

$$u = \frac{\partial \psi}{\partial y} = 2y \Rightarrow \psi = y^2 + f(x) \quad (1)$$

$$v = -\frac{\partial \psi}{\partial x} = 4x \Rightarrow \frac{\partial \psi}{\partial x} = -4x \quad (2)$$

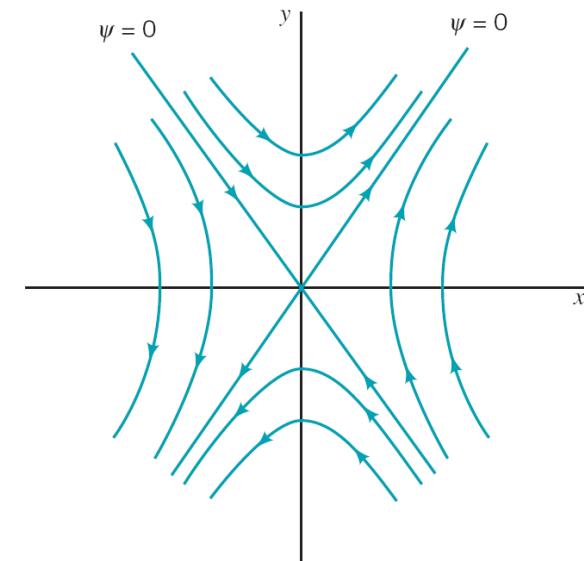
$$(1) \wedge (2) \Rightarrow \frac{df}{dx} = -4x \Rightarrow f = -2x^2 + c \quad (3)$$

$c$  is arbitrary; let  $c=0$  for simplicity

$$(1) \wedge (3) \Rightarrow \underline{\underline{\psi = y^2 - 2x^2}}$$

$$\text{For } \psi = 0 \Rightarrow y^2 - 2x^2 = 0 \Rightarrow y = \pm \sqrt{2}x$$

$$\text{In general, } \underline{\underline{\frac{y^2}{\psi} - \frac{x^2}{\psi/2} = 1}} \quad \text{hyperbola}$$



Direction of flow:  
 $v = 4x$

So, for  $x > 0$  flow is upwards